

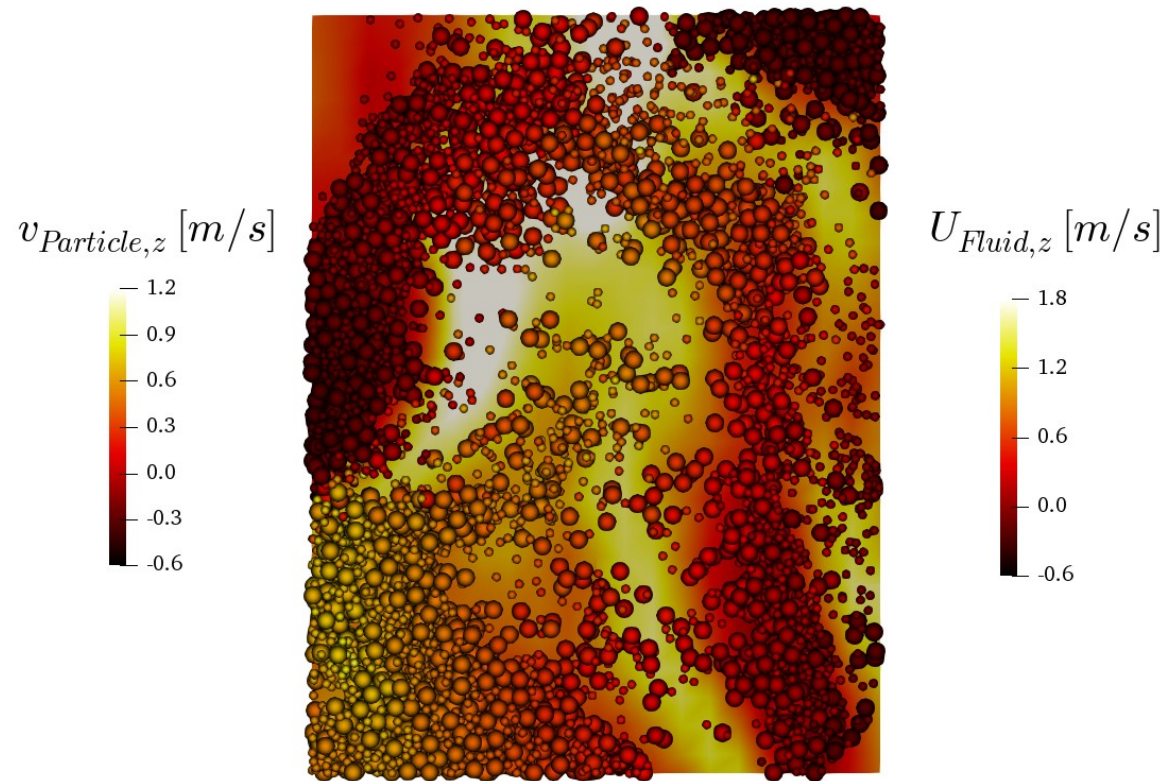
Modeling Cohesive Gas- Particle Flows

with a Parcel-Based
Lagrangian Approach

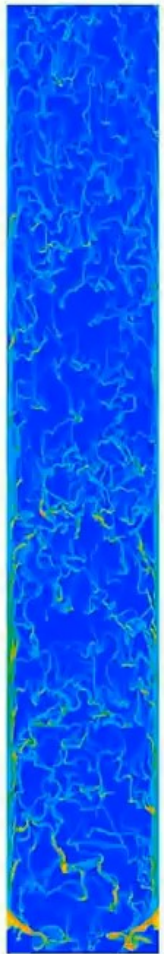
Stefan Radl,
Josef Tausendschön

Institute of Process
and Particle Technology
AIChE Annual Meeting 2019

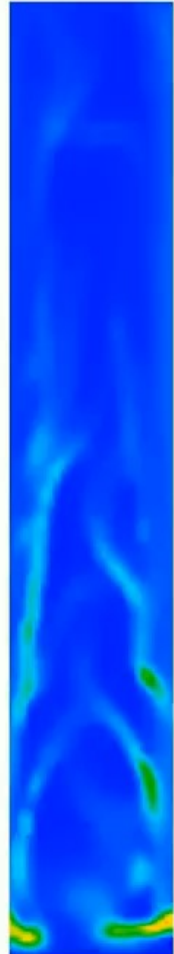
17+3 mins



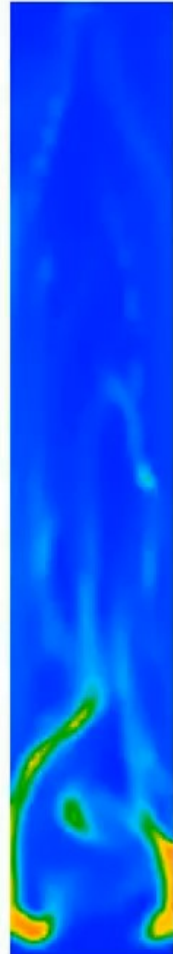
Motivation



Resolved TFM
0.625 mm



fTFM - 10 mm
1M Anisotropic

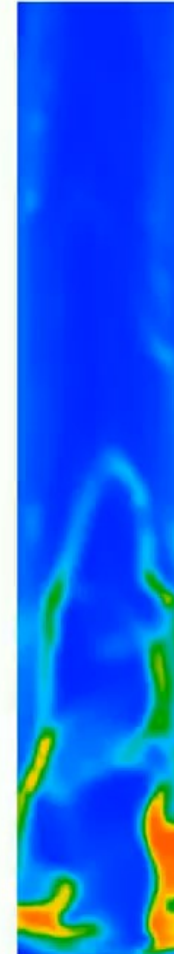


fTFM - 10 mm
2M Anisotropic



fTFM - 10 mm
3M Anisotropic

New approach: correction depends on
direction



fTFM - 10 mm
2M Isotropic

Classical approach: correction
identical in each direction

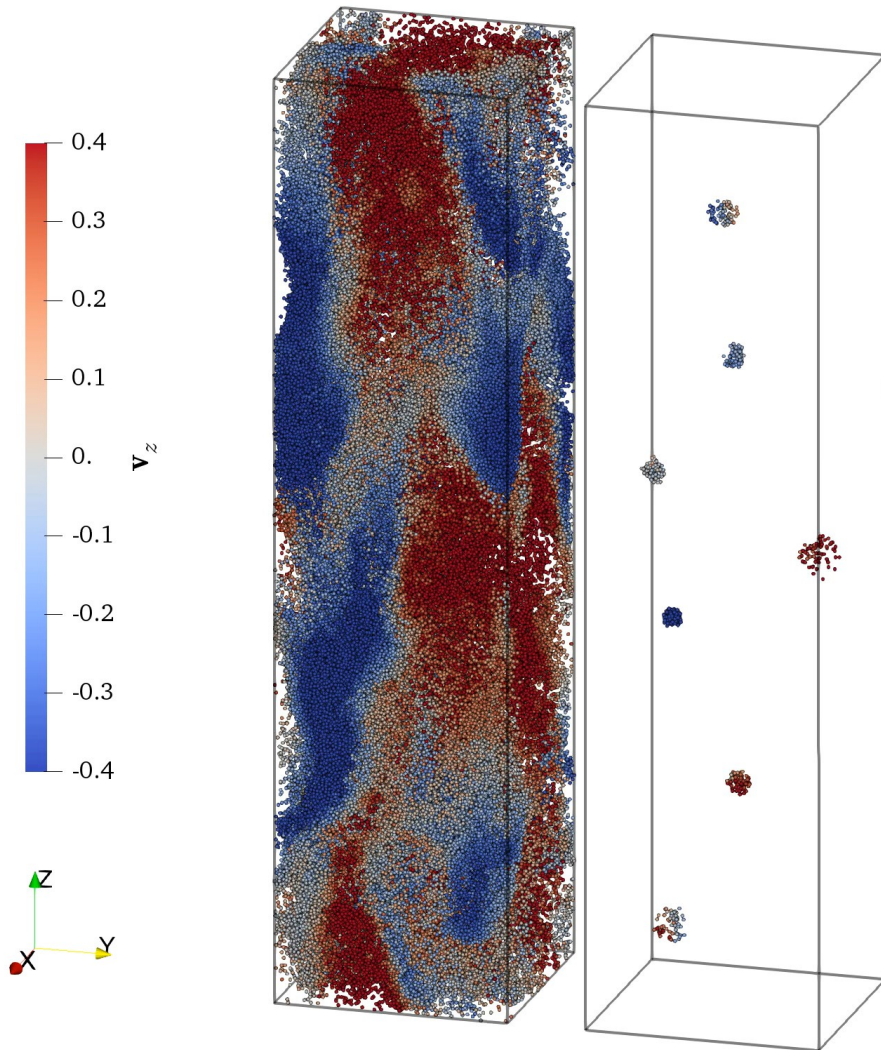
On the large scale: a **filtered model** is needed (e.g., filtered TFM)

Improved „meso scale“ closures (drag, stress) are needed

Q1: How do these closures look like for **cohesive & polydisperse** powders?

Q2: Is a filtered „CFD-parcel“ (Lagrangian) approach feasible?

Coarse-Graining Basics



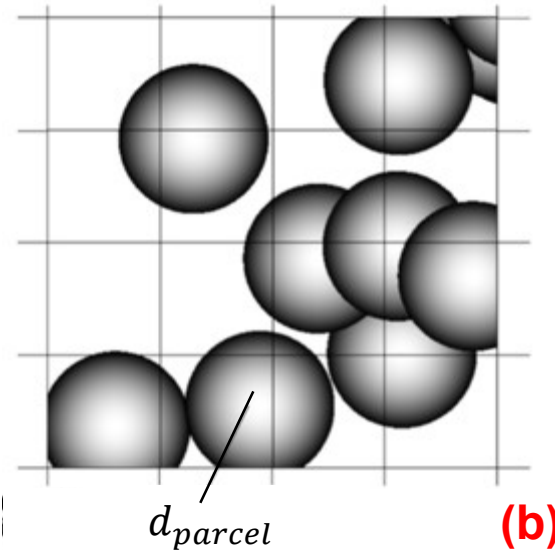
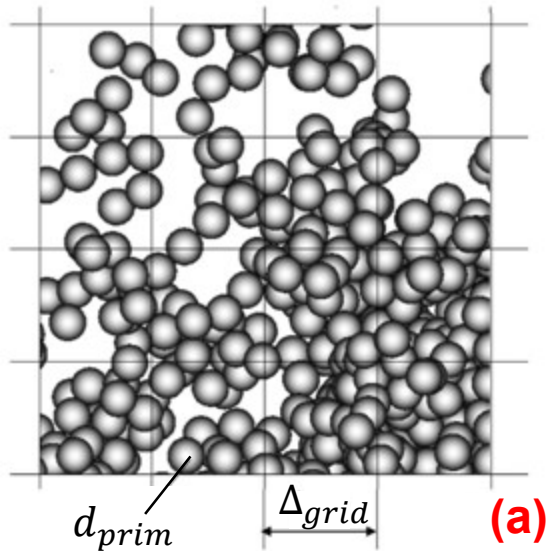
A parcel is...

- approximation of a **particle ensemble**
- representation of a **fixed number of particles**, but not a fixed set
- **cannot directly predict particle-particle collisions**
→ approximate “**parcel collisions**”

Coarse-Graining Basics

- **Coarse Graining of the Particles:**

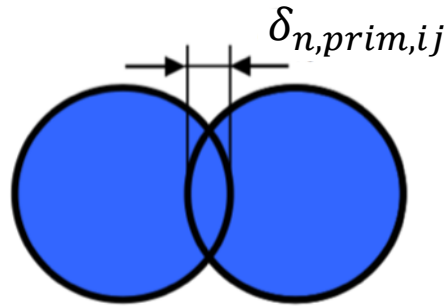
$d_{parcel} = \alpha \cdot d_{prim} \Rightarrow$ one parcel consists of α^3 primary particles



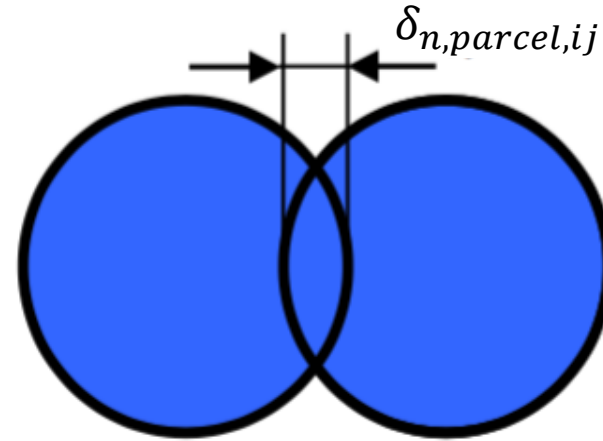
- **With a fixed CFD grid size, parcels can become bigger than a CFD cell!**

\Rightarrow typically, CFD cell size is increased for $\alpha > 1$

Coarse-Graining Basics



$$F_{c,prim,ij} = k_{n,prim} \delta_{n,prim,ij} + c_{n,prim} \dot{\delta}_{n,prim,ij}$$



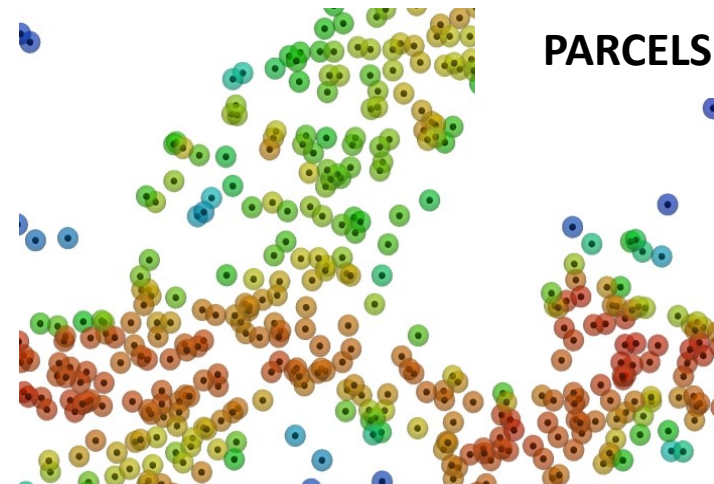
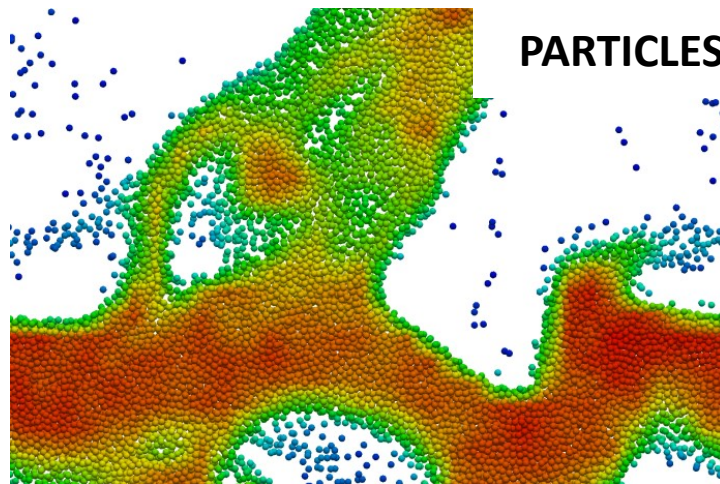
$$F_{c,parcel,ij} = k_{n,parcel} \delta_{n,parcel,ij} + c_{n,parcel} \dot{\delta}_{n,parcel,ij}$$

- we suggest a scaling of contact and cohesive forces based on **constant stress**:

$$\text{Force}/R^2 = \text{const.}, \text{ leads to } \left\{ \begin{array}{l} \gamma_{prim} \cdot \alpha = \gamma_{parcel} \\ \mu_{liq,prim} \cdot \alpha = \mu_{liq,parcel} \\ k_{n,prim} \cdot \alpha = k_{n,parcel} \\ c_{n,prim} \cdot \alpha^2 = c_{n,parcel} \\ A_{prim} \cdot \alpha^3 = A_{parcel} \end{array} \right.$$

k_n = Particle Stiffness
c_n = Normal Damping coeff.
γ = Surface Tension
μ_l = Liquid Viscosity
A = Hamaker const.

Can we predict Stress?



$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^{cont} + \boldsymbol{\sigma}^{kin} = \boldsymbol{\sigma}(\mathbf{u}_p, \phi_p, T, d_{prim}, e_p, \mathbf{f}_{coh})$$

$$\boldsymbol{\sigma}^{cont} = \frac{1}{V} \sum_{p \in p_V} \sum_{j \in C_p} \frac{1}{2} \mathbf{r}_{pj} \mathbf{F}_{pj}$$

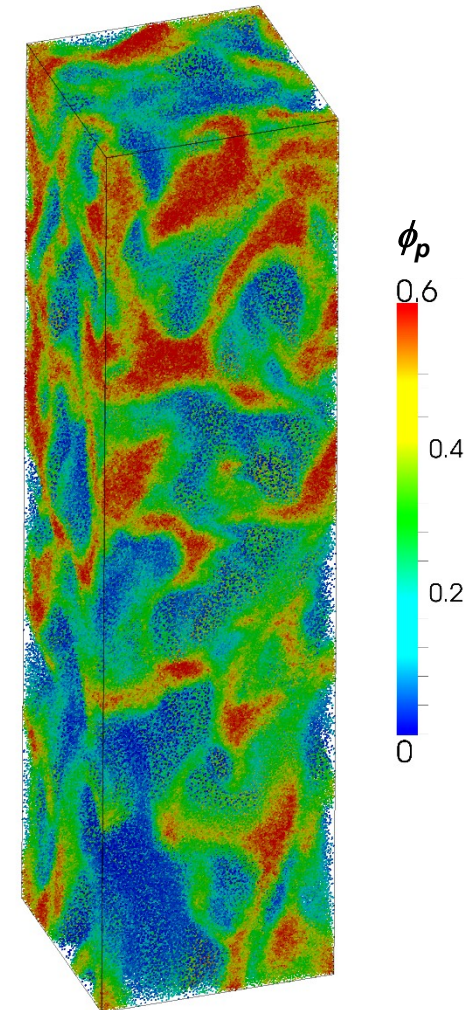
$$\boldsymbol{\sigma}^{kin} = \frac{1}{V} \sum_{p \in p_V} m_p (\mathbf{v}_p - \bar{\mathbf{v}}_p)(\mathbf{v}_p - \bar{\mathbf{v}}_p)$$

- Setup

- Gas-particle system ($\rho_p/\rho_f \approx 1000$), freely sedimenting.
- Low Re system ($u_t = 0.22$ m/s, $Re_p \approx 1$).
- 3D, size: **8x32 mm** & 4x16 mm, **periodic**.

- Fluid Grid & Coarse Graining Sensitivity

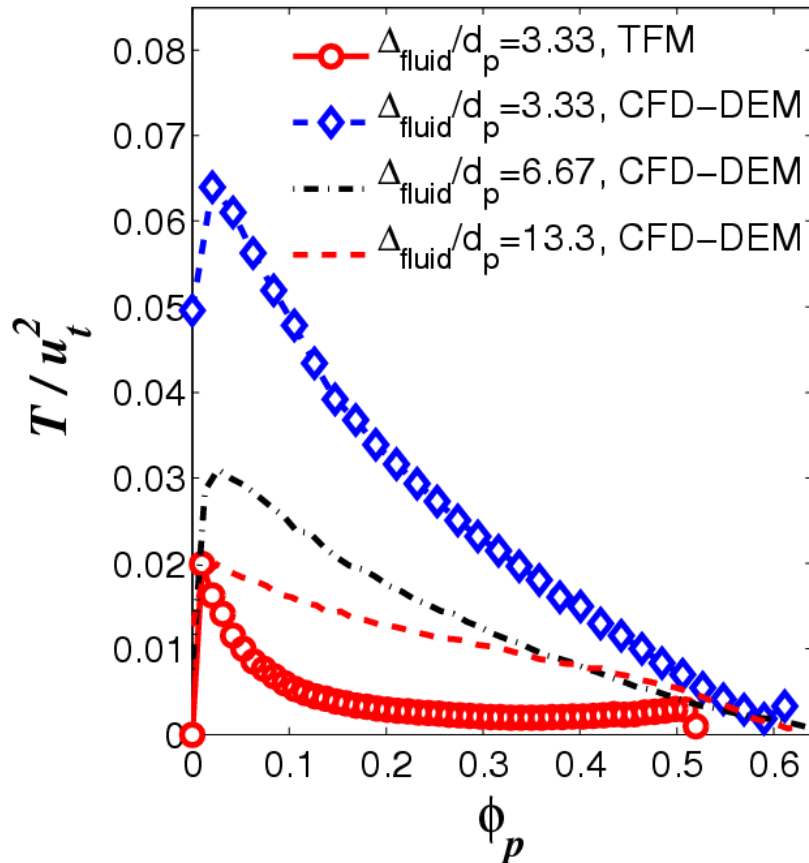
- Analyze distribution of granular **temperature and pressure** to illustrate effect of grid resolution
- Investigate effect of **coarse graining** (on coarse grids!)



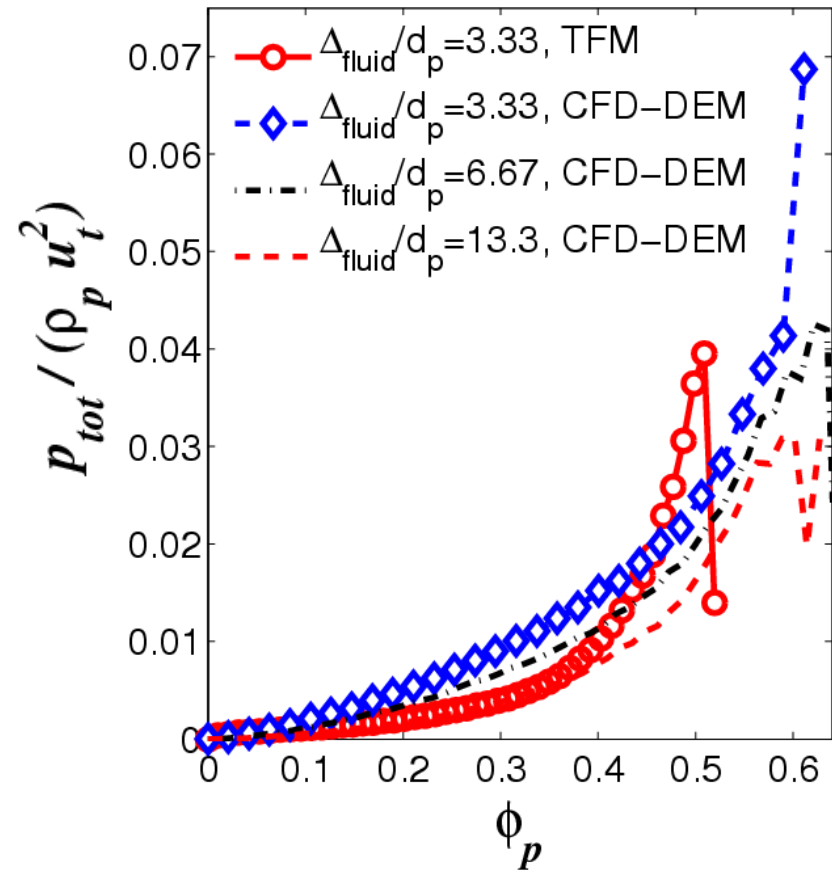
Clustering predicted by CFD-DEM
($2.3 \cdot 10^6$ particles, $\langle \phi_p \rangle = 0.25$).

Stress Prediction

- Gran. Temperature and Particle-Phase Pressure

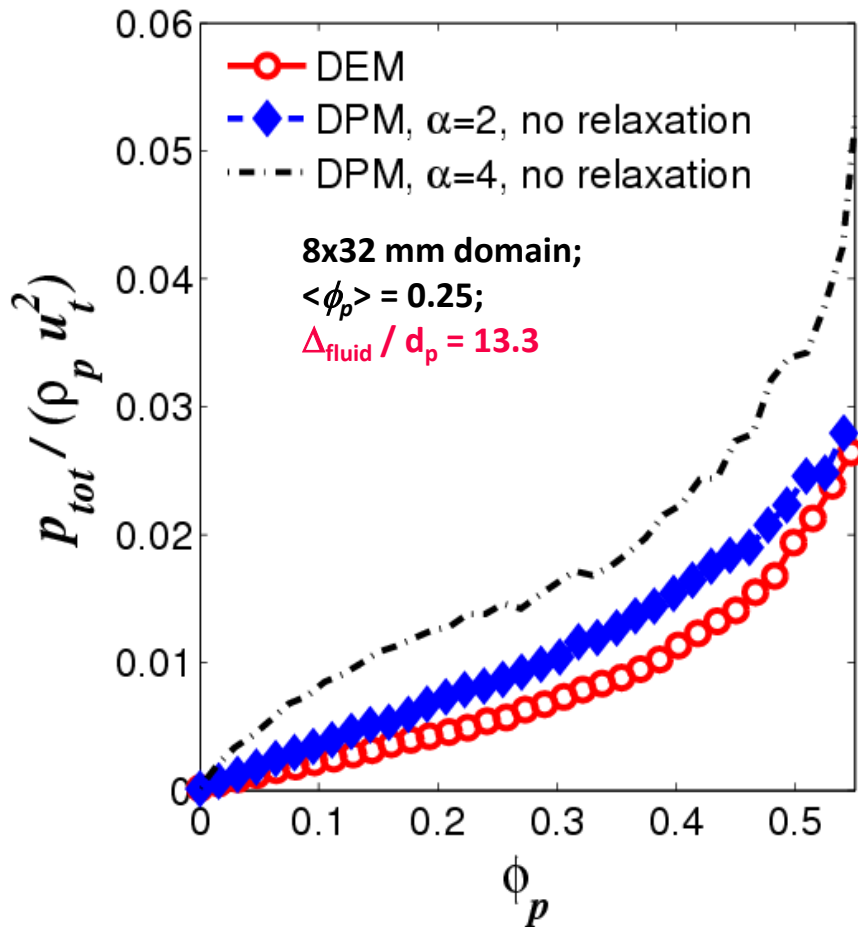


- T and **stress** quantitatively sensitive to grid resolution



- **TFM** significantly off

- Comparison DEM and Coarse Grained DEM



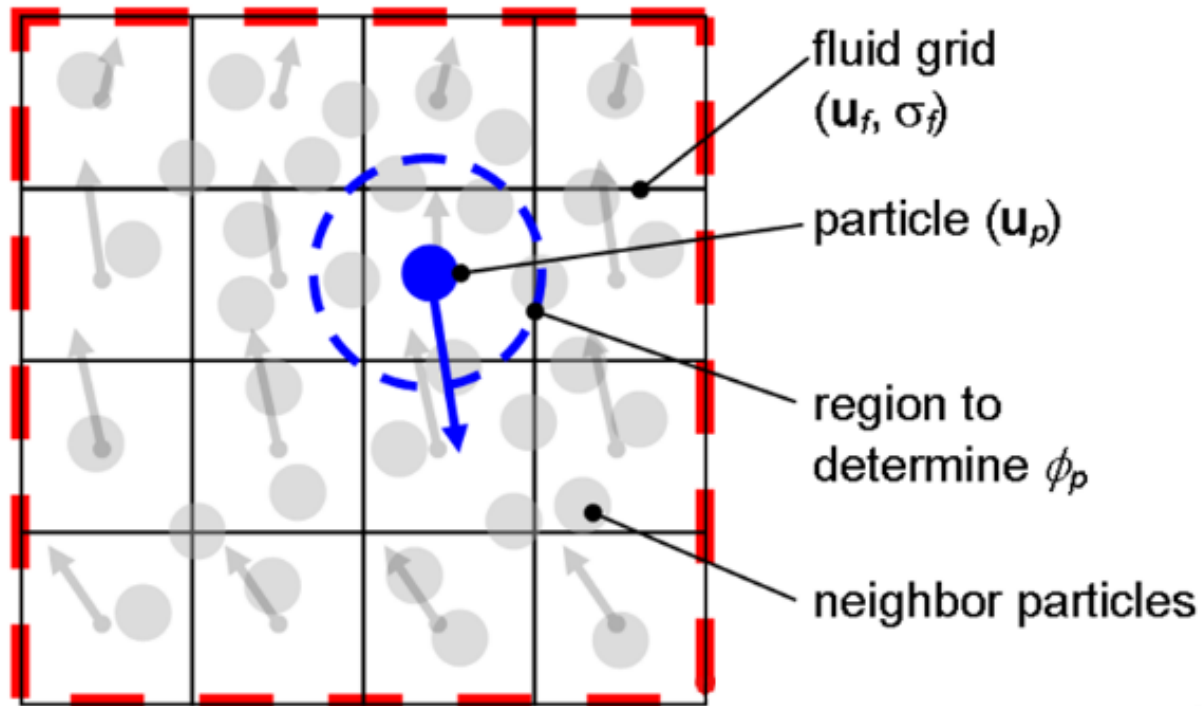
- **Particle-phase Pressure**

- stress increases with increasing parcel size as expected from shear-flow simulations

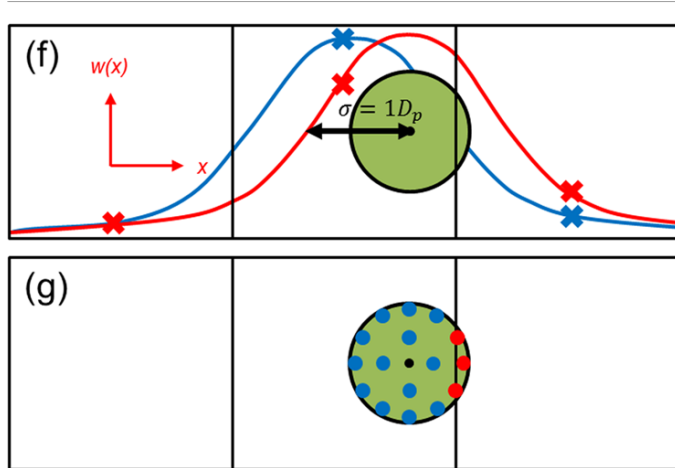
However,

→ ...this is for a coarse grid! We need **smoothing** for a fair comparison

Smoothing Strategy



Smoothing Basics

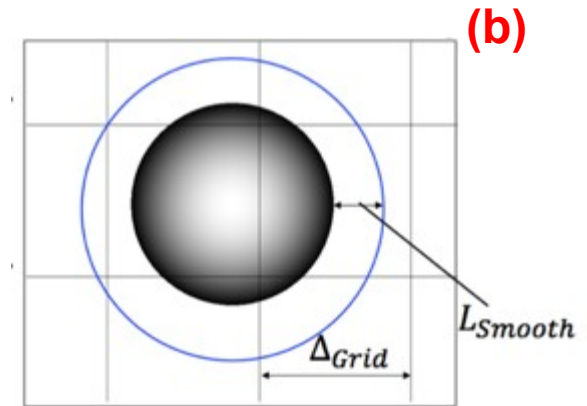


(a)³

Combination of
these two
schemes



Diffusive Smoothing

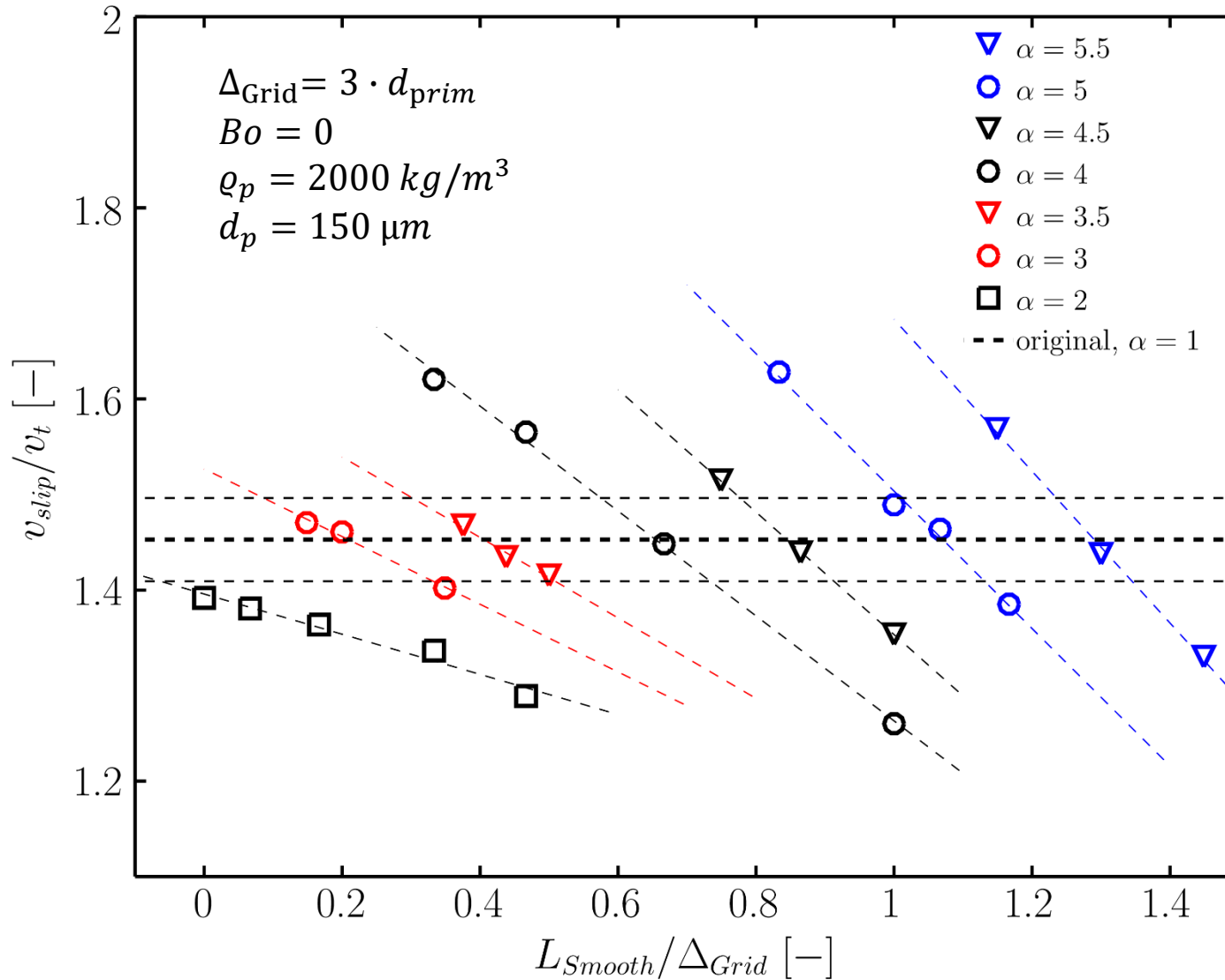


- **Smoothing operation** is performed via (an implicit) solution of a diffusion equation for each transferred quantity ψ :

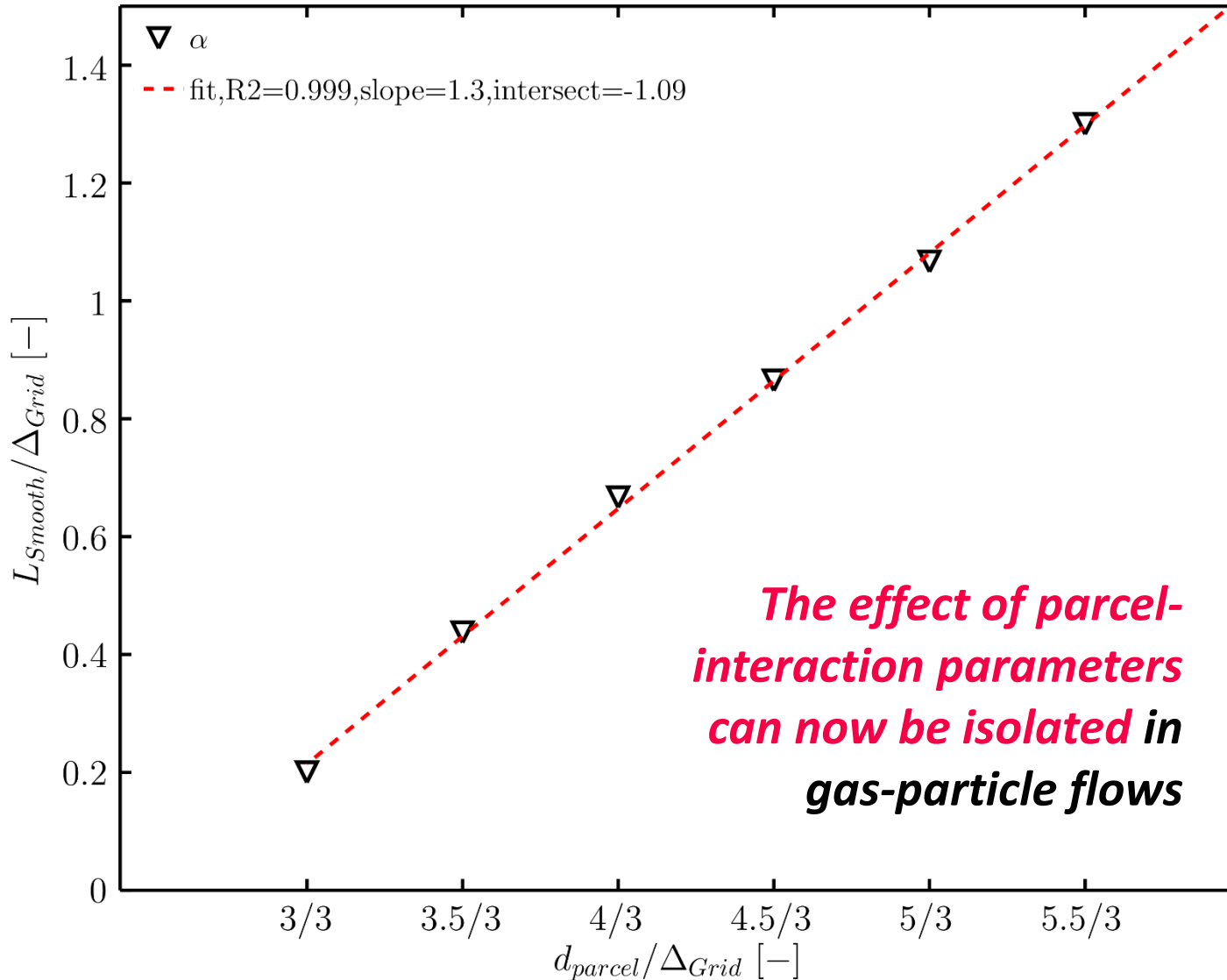
$$\frac{\partial \psi}{\partial t} = D \nabla^2 \psi \quad , \quad D = L_{Smooth}^2 / \Delta t$$

Optimal Smoothing Length

*Non-cohesive &
Monodisperse*



Optimal Smoothing Length

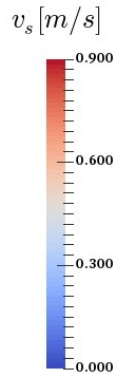


Non-cohesive & Monodisperse

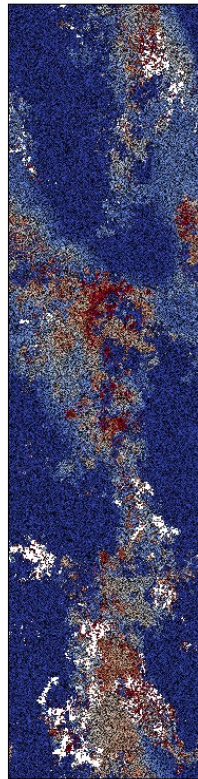
The effect of parcel-interaction parameters can now be isolated in gas-particle flows

Cohesion & Coarse Graining

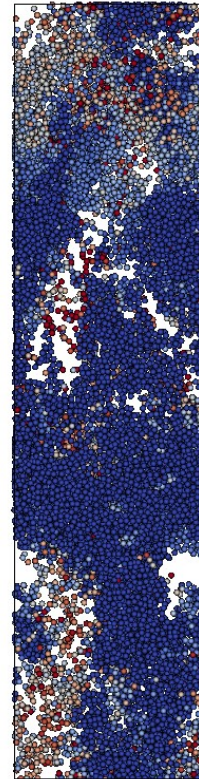
Time: 3.52 s



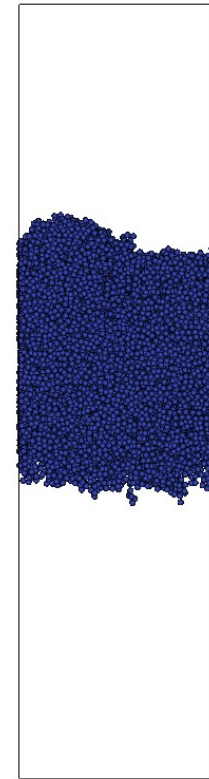
original
system
 $Bo = 50$



$\alpha = 4$
Stress
 $Bo = 50$



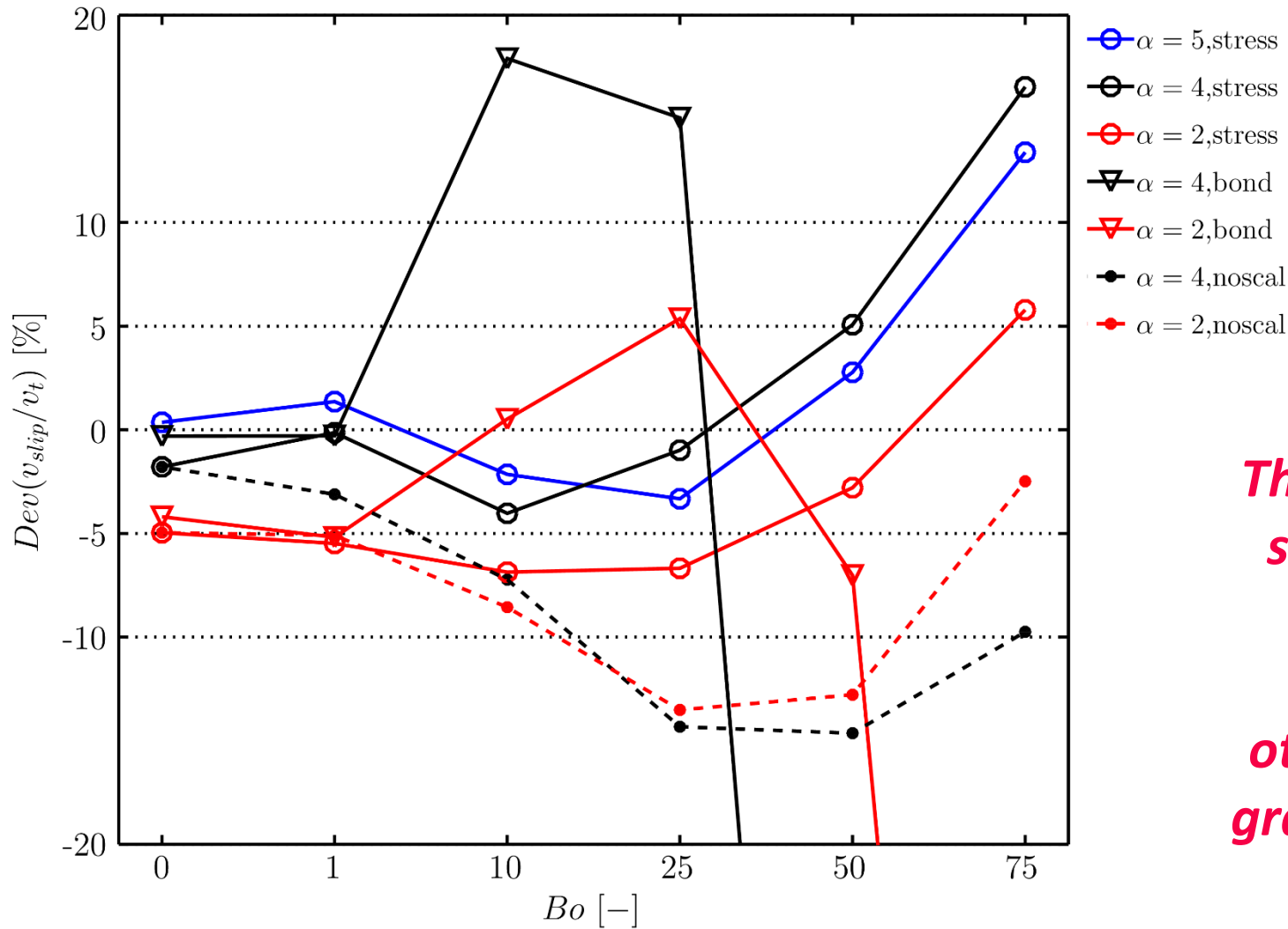
$\alpha = 4$
Bond
 $Bo = 50$



$$Bo = \frac{6 \gamma}{d_p^2 g \rho_p}$$

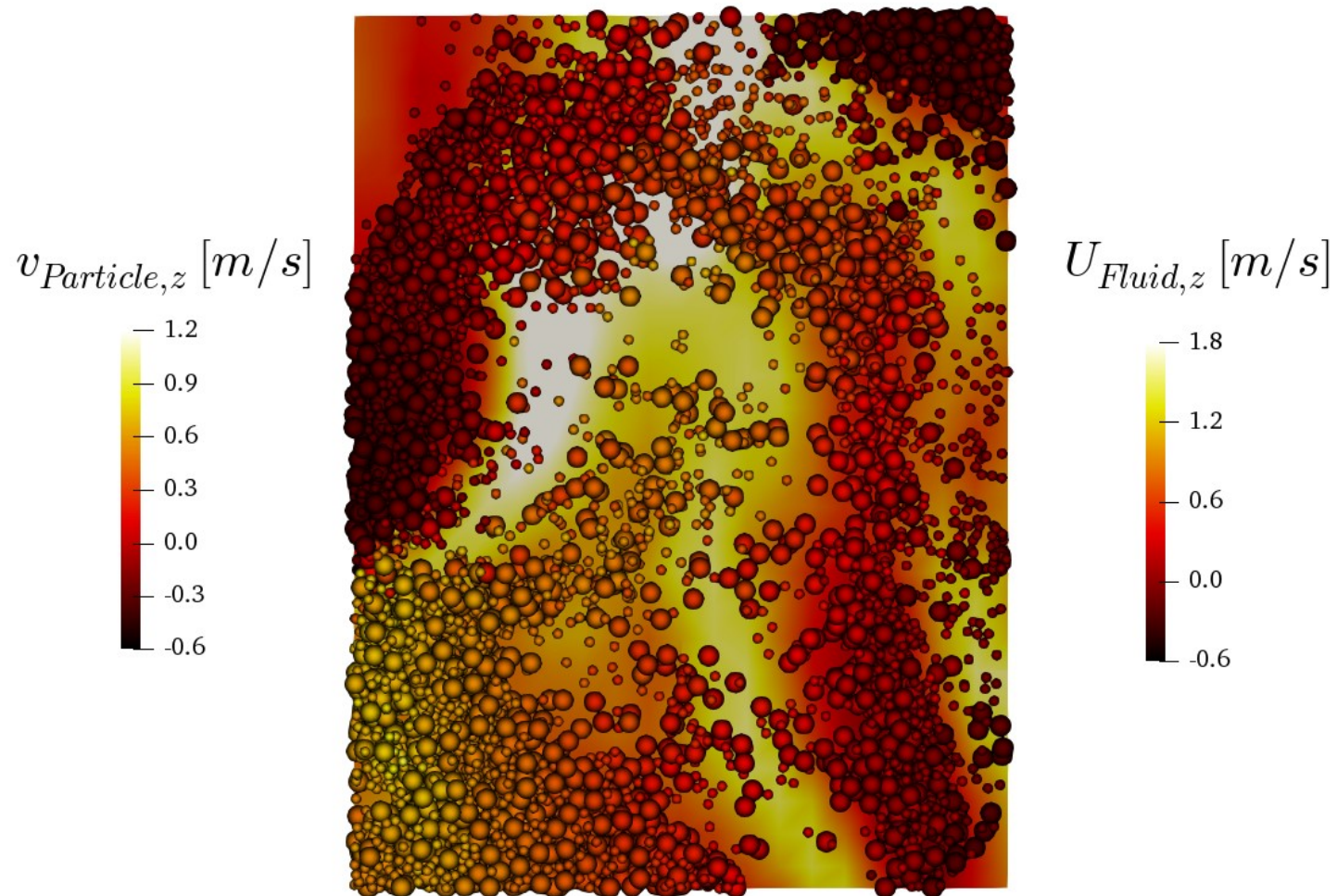
Cohesion

*wet
particles*



*The proposed
stress-based
scaling is
superior to
other coarse-
graining force
models*

Outlook & Conclusion

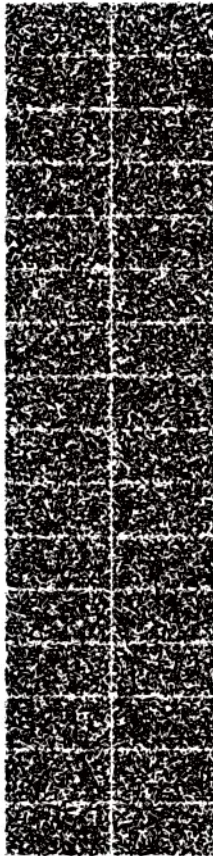
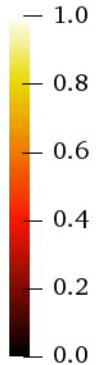


Polydispersity

Primary Particle
System

Time: 0.01 s

$v_{Particle,z}$ [m/s]



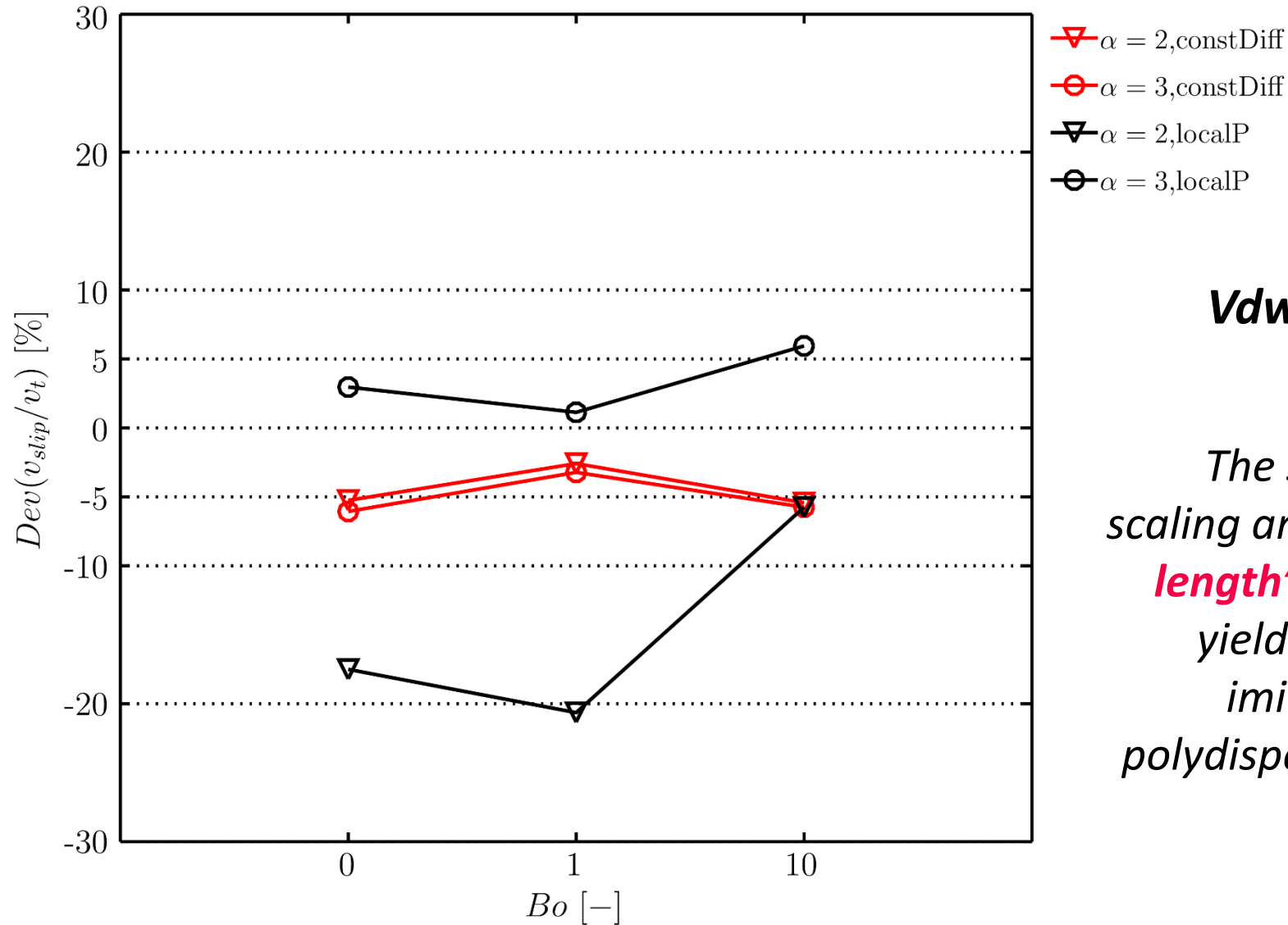
$\alpha = 2$
const.Diff.
smoothing



$\alpha = 2$
local P.size
smoothing



Polydispersity



Vdw-cohesion

The stress-based scaling and “constant length” smoothing yield an accurate imitation of the polydisperse primary system

- With smoothing operation and optimal smoothing lengths: **effect of parcel-interaction parameters can be isolated**
- **Stress-based scaling** led to a very accurate imitation (of sedimentation speed!) of the original system in the monodisperse setup
- **$Bo = 50$ and $\alpha = 5$** maximum permissible parameters to guarantee acceptable deviation from original system
- Stress-based scaling and **smoothing** appears suitable for **polydisperse systems** as well

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Thank you!

Special thanks to
Jari Kolehmainen and Sundar

