

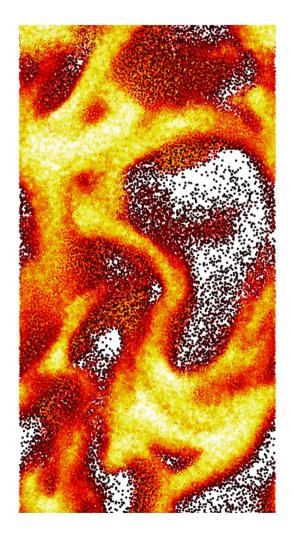


### Coarse-Grid Simulations Using Parcels An Advanced Drag Model based on Filtered

CFD-DEM Data

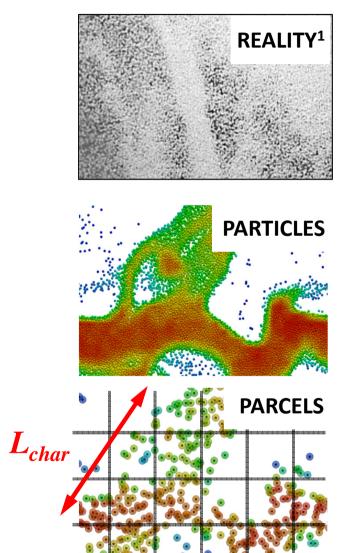
<u>Stefan Radl</u> and Sankaran Sundaresan

Talk 5-4 Fluidization XIV Noordwijkerhout, The Netherlands



# Outline

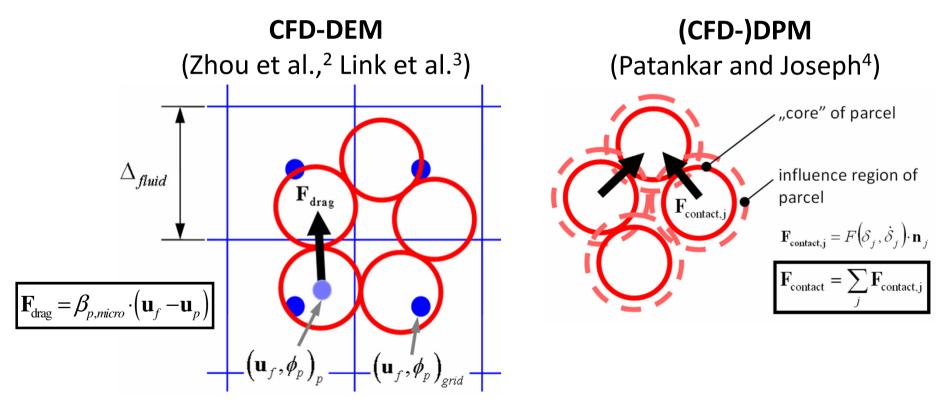
- Motivation
- Simulation Setup
- Drag Model Results
- A Short Review of Important Length Scales



<sup>1</sup>Courtesy: Franklin Shaffer, NETL, Morgantown, WV (2009).

### **Simulation Setup**

- In the CFD-DEM<sup>2,3</sup> the fluid flow is calculated on a **computational grid that is larger than the particles "microscopic" drag law**.
- In the CFD-DPM one computes virtual "contact" forces via a DEM-like tracking of parcel collisions.<sup>4</sup> Microscopic draw law often not suitable.



**Simulation Setup** 

$$\nabla p = \nabla p_{dyn} + \rho_{mix} \mathbf{g}$$

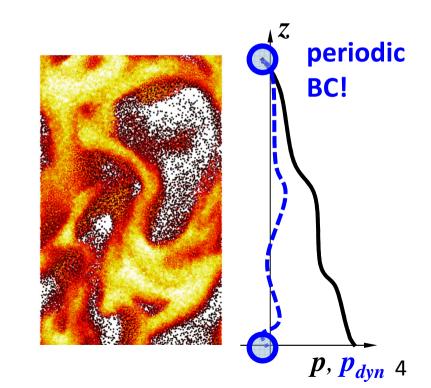
**Momentum Balance Equation in a Periodic Box** 

 $\partial_t \left( \phi_f \rho_f \mathbf{u}_f \right) + \nabla \cdot \left( \phi_f \rho_f \mathbf{u}_f \mathbf{u}_f \right) = -\phi_f \cdot \nabla p - \nabla \cdot \left( \phi_f \cdot \mathbf{\tau}_f \right) + \phi_f \rho_f \mathbf{g} + \mathbf{\Phi}_f \mathbf{g}$ 

 $\partial_t \left( \phi_f \rho_f \mathbf{u}_f \right) + \nabla \cdot \left( \phi_f \rho_f \mathbf{u}_f \mathbf{u}_f \right) = -\phi_f \cdot \nabla p_{dyn} - \nabla \cdot \left( \phi_f \cdot \boldsymbol{\tau}_f \right) + \phi_f \left( \rho_f - \rho_{mix} \right) \mathbf{g} + \Phi$ 

...pressure "as usual", but with different meaning!

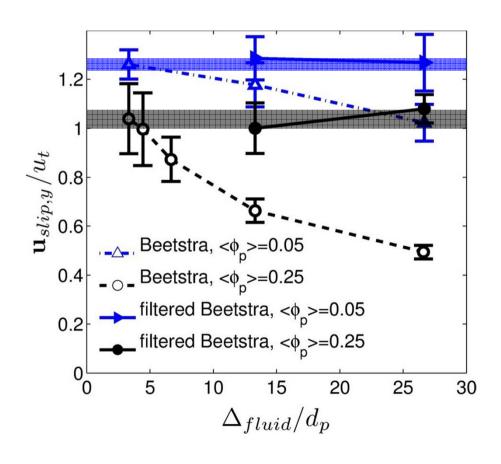
...treat as explicit term in the fluid's momentum balance equation



- 1. CFD-DEM
  - Fine fluid grid
  - Track all the particles
  - Micro-scale drag law
  - Obtain filtered drag law
- 2. Coarse Grid CFD-DEM
  - Coarse fluid grid
  - Track all the particles
  - Use filtered drag law

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# Q: Do **CFD-DEM** and **Coarse Grid CFD-DEM** yield the same results?

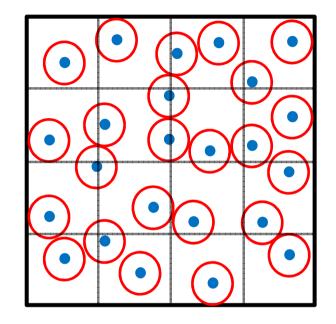


- Large decrease of slip velocity if using "microscopic" drag law (Beetstra; -53% for  $\langle \phi_p \rangle = 0.25$ ).
- Coarse Grid CFD-DEM with filtered drag law is within
  +2% (<φ<sub>p</sub>>=0.05) and
  ±3.8% (<φ<sub>p</sub>>=0.25) of wellresolved CFD-DEM!

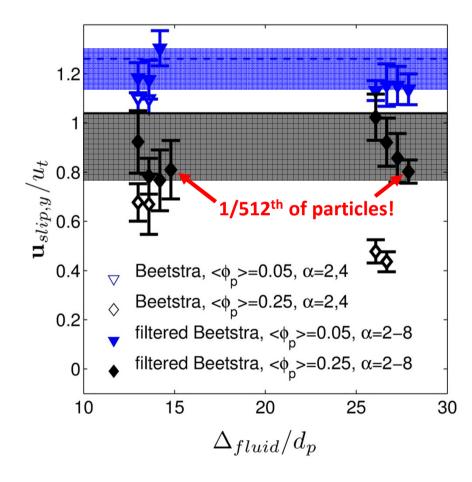
75 μm particles, 8 x 32 x 8 mm domain, 0.46M - 2.32M particles.

- 3. CFD-DPM
  - Use filtered drag law
  - Coarse fluid grids
  - Track parcels of size

 $d_p = \alpha d_{prim}$ 



#### Q: Do **CFD-DEM** and **CFD-DPM** yield the same results?



- CFD-DPM with "microscopic" drag law significantly under-predicts slip (-58% for <φ<sub>p</sub>>=0.25).
- Filtered drag law improves results, but still significant under prediction: -22% ( $<\phi_p>=0.25$ )
- Now, we introduce a correction to account for parcel size effects:

$$c_{corr} = \exp\left[-k\left(\alpha - 1\right)\right]$$

k = 0.05 (based on calibration)

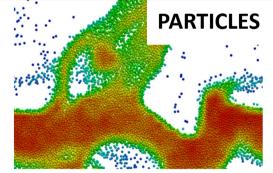
75 μm particles, 8 x 32 x 8 mm domain, 0.46M -2.32M particles, pairs of symbols represent CFD-DPM result, horizontal lines are results of wellresolved CFD-DEM simulations.

# Outline

- Motivation
- Simulation Setup
- Drag Model Results
- A Short Review of Important Length Scales
  - What is the effective force on an ensemble of particles?
  - ➤ What is the characteristic size of a particle cluster... ...to make Δ<sub>fluid</sub> dimensionless?

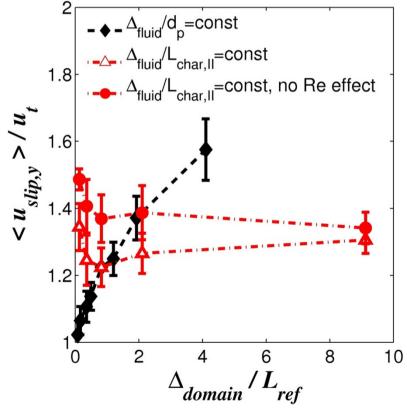
<sup>1</sup>Courtesy: Franklin Shaffer, NETL, Morgantown, WV (2009).

$$\frac{\overline{\beta}_{p}}{\beta_{p,micro}} = c_{corr} \left( \alpha \right) \left[ 1 - f \left( \Delta_{fluid}, \overline{\phi}_{p} \right) h \left( \overline{\phi}_{p} \right) \right]$$



### Drag Model Tests (CFD-DEM)

• Test 1: Use  $d_p$  or  $L_{char,II} = u_t^2 / g Fr_p^{-2/3} = const$  and test sensitivity to  $L_{ref} = u_t^2 / g$  •  $\Delta_{fluid}/d_p = const$  does NOT

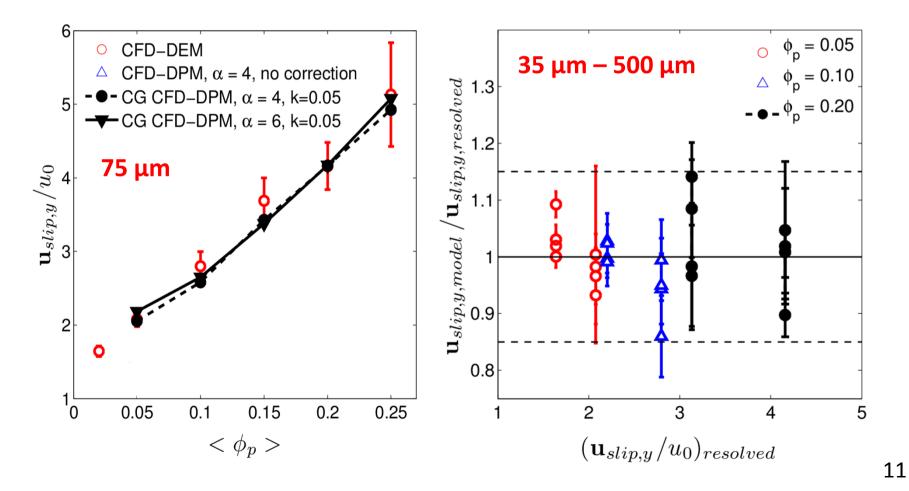


- $\Delta_{fluid}/d_p$  = const does NOT yield results independent of  $L_{ref}$ . Same is true for  $\Delta_{fluid}/d_p$  = const.
- Δ<sub>fluid</sub>/L<sub>char,II</sub> = const works much better! This is true with/without Reynolds number dependent drag.
- L<sub>char,II</sub> seems to be a useful reference length WHY?

Domain-averaged slip velocity for constant  $L_{char,II}$ , and variation of particle diameter & density ( $\langle \phi_D \rangle = 0.05$ ).

### **Drag Model Tests**

• Test 2: Use  $L_{char,II} = u_t^2 / g Fr_p^{-2/3} = const$  and test sensitivity to  $d_{prim}$  and  $d_p$  for various  $\langle \phi_p \rangle$ 



### **Review of Length Scales**

#### **Inspiration from Continuum-Based Theory**

• Particle-Phase Momentum Balance\*

$$\rho_p u_t^2 \left[ \frac{1}{u_t} \partial_t (\phi_p \mathbf{u}_p^*) + \nabla \cdot (\phi_p \mathbf{u}_p^* \mathbf{u}_p^*) \right] = -\nabla \cdot \boldsymbol{\sigma}_p - \phi_p \nabla \cdot \boldsymbol{\sigma}_g + \beta u_t \mathbf{u}_{slip}^* + \rho_p \phi_p g \mathbf{g}^*$$

• **Estimate** for the **granular temperature** (shear production vs. dissipation)  $d_n$ 

$$\sqrt{T} \approx \frac{d_p}{L_{visc,II}} u_t$$

A length scale based on the balance of *viscous particle stress* & gravity is:

$$L_{visc,II}{}^{3}\mathbf{g}^{*} = \left(\frac{u_{t}^{2}}{g}\right)^{3} \left(\frac{d_{p}g}{u_{t}^{2}}\right)^{2} \frac{1}{\phi_{p}} \cdot \nabla^{*} \cdot \left[2C_{KT}F_{diss}{}^{*}\left(\nabla^{*}\mathbf{u}_{p}^{*} + \nabla\mathbf{u}_{p}^{*T}\right)\right] \qquad \mathbf{n} = -2/3$$

### Summary

- The advanced drag model takes the effect of grid resolution, parcels size, local particle concentration and particle properties into account. It is valid for flow situations far away from walls.
- For the smallest length relevant for particle clustering, our simulations suggest (tested for  $Re_p = O(1)...O(100)$ ):

$$L_{char,II} = \frac{u_t^2}{g} F r_p^{-2/3}$$

 L<sub>char,II</sub> appears to be the key reference length scale for the fluid grid size in coarse-grid simulations, in case particle inertia is not that important (compared to ρ<sub>p</sub>T).





#### **Coarse-Grid Simulations Using Parcels**

## An Advanced Drag Model based on Filtered CFD-DEM Data

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