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# OPENCFS-DATA: IMPLEMENTATION OF THE STOCHASTIC NOISE GENERATION AND RADIATION MODEL (SNGR)

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## ABSTRACT

Preliminary aeroacoustic investigations in competitive industries require rapid numerical simulation techniques to gain initial insight into the flow and acoustic field. Although there are capabilities to resolve virtually all turbulence length scales, these techniques are often impractical in early stages of component development. Therefore, the flow field is typically assessed by a Reynolds-averaged Navier Stokes Simulation. Building upon the results of that flow simulation, a stochastic approach to reconstruct the turbulent velocity fluctuations. In conjunction with a hybrid aeroacoustic workflow, this approach is useful in early stage virtual prototyping of aeroacoustic applications. In this working paper, we present the SNGR algorithm of CFS-Data, the open-source pre-post-processing part of openCFS, with a focus on the computation of aeroacoustic sources.

**Keywords** Open Source FEM Software · Multiphysics Simulation · C++ · Acoustics · Aero-Acoustics · openCFS · SNGR

## 1 Introduction

Within this contribution, we concentrate on the openCFS [32] module *openCFS-Data* [33], the implemented SNGR method called *syntheticTurbulence\_SNGR* and potential model applications. The method was initially applied in [46, 47] and more details on a first application can be found there. Stochastic methods constitute a low-cost computational fluid dynamics (CFD) approach to reconstruct the turbulent velocity fluctuations using results Reynolds-averaged Navier-Stokes (RANS) simulations. This approach was introduced by Béchara et al. [2] in 1994 and is known as stochastic noise generation and radiation (SNGR). Regarding the model in [46], it was applied to a cavity noise simulation using a hybrid aeroacoustic workflow [39, 24, 40]. The derivatives of the Lighthill's source term were computed by a radial basis function scheme [23, 36]. Using recently developed equations, the method can potentially be applied to aeroacoustic formulations based on the acoustic potential [26, 19] in combination with a Helmholtz decomposition [35, 34, 25, 30]. Furthermore, this methodology can be valuable for automotive OEMs since it poses a fast estimate on the flow-acoustic properties of broadband noise excitation which can be applied as loading [4, 6, 28, 47, 17]. Furthermore, the hybrid aeroacoustic workflow was found to be useful for fan noise computations [22, 41, 38, 42, 43, 21], the noise emissions of the turbocharger compressor [8, 9, 7], the acoustics of fluid-structure-acoustic-interaction processes [37, 44, 48, 29, 5, 14, 16, 31, 15, 20, 12]. Potential nonphysical behavior generated with the source computation can be identified using [27]. For a literature overview on the developments connecting to SNGR, have a look at the article [13].

## 2 Stochastic Noise Generation and Radiation

As proposed by Kraichnan [11] and Karweit et al. [10] a spatially stochastic turbulent velocity field can be generated as a finite sum of  $N$  statistically independent random Fourier mode

$$\mathbf{u}_t(\mathbf{x}) = 2 \sum_{n=1}^N \tilde{u}_n \cos(\mathbf{k}_n \cdot \mathbf{x} + \psi_n) \boldsymbol{\sigma}_n, \quad (1)$$

where  $\mathbf{x}$  is the spatial position, and  $\mathbf{k}_n$ ,  $\tilde{u}_n$ ,  $\psi_n$ , and  $\boldsymbol{\sigma}_n$  are the wave vector, the amplitude, the phase, and the direction of the  $n^{\text{th}}$  mode, respectively. The wave vector  $\mathbf{k}_n$  is randomly chosen on a sphere of radius  $k_n$  to ensure isotropy. Additionally, incompressibility of the turbulent flow field implies  $\partial u_{ti}/\partial x_i = 0$  and hence

$$\mathbf{k}_n \cdot \boldsymbol{\sigma}_n = 0 \quad \text{for } n = 1, \dots, N \quad (2)$$

The turbulent kinetic energy  $K$  is computed as the statistical mean of  $1/2 u_{ti} u_{ti}$  and may thus be written with Eq. (1) as

$$K = \sum_{n=1}^N \tilde{u}_n^2. \quad (3)$$

A homogeneous isotropic turbulence is characterized by a three-dimensional energy spectrum  $E(k)$  which allows to compute the turbulent kinetic energy by

$$\int_0^\infty E(k) dk = K. \quad (4)$$

Moreover, the spectrum  $E(k)$  allows computing the rate of dissipation of turbulence energy  $\epsilon$  by

$$2\nu \int_0^\infty k^2 E(k) dk = \epsilon, \quad (5)$$

where  $\nu$  is the kinematic viscosity. Discretizing Eq. (4) and combining it with Eq. (3) yields

$$\tilde{u}_n = \sqrt{E(k_n) \Delta k_n}. \quad (6)$$

The spectrum  $E(k)$  used to simulate the complete spectral range is a von Kármán-Pao spectrum [45, 18]

$$E(k) = \alpha \frac{u'^2}{k_e} \frac{(k/k_e)^4}{[1 + (k/k_e)^2]^{17/6}} \exp \left[ -2 \left( \frac{k}{k_\eta} \right)^2 \right], \quad (7)$$

where  $k_\eta = (\epsilon/\nu^3)^{1/4}$  is the Kolmogorov wave number, and  $u' = \sqrt{2K/3}$  is the root-mean-square value of the velocity fluctuations. Assuming that the turbulent kinetic energy  $K$  and the rate of dissipation of turbulence energy  $\epsilon$  are known from the computational fluid dynamics (CFD) solution, and inserting Eq. (8) into Eq. (4) yields

$$\alpha = \frac{55}{9\sqrt{\pi}} \frac{\Gamma(\frac{5}{6})}{\Gamma(\frac{1}{3})} \approx 1.45276. \quad (8)$$

To compute the wave number  $k_e$  of the most energetic eddies corresponding to the maximum of the energy spectrum  $E(k)$ , Eq. (8) is inserted into Eq. (5), which leads to

$$\frac{u'^3}{\epsilon} = \frac{2}{k_e} \left[ \alpha \Gamma \left( \frac{2}{3} \right) \right]^{-\frac{3}{2}} \approx 0.725 \frac{1}{k_e} \quad (9)$$

when  $k_e/k_\eta \rightarrow 0$ . To achieve a better discretization of the power in the lower wave number range corresponding to the larger energy-containing eddies, a logarithmic distribution of the  $N$  wave numbers is used. A logarithmic step of such a distribution reads

$$\Delta k_1 = \frac{\log k_N - \log k_1}{N - 1} \quad (10)$$

and hence the  $n^{\text{th}}$  wave number  $k_n$  is given by

$$k_n = \exp [\log k_1 + (n - 1) \log \Delta k_1]. \quad (11)$$

Since this method only models spatial correlation but not temporal correlation, Bailly et al. [1] included time-dependence in Eq. (1) to arrive at reasonable statistical properties. Hence, the turbulent velocity field is now computed as a sum of unsteady random Fourier modes

$$\mathbf{u}_t(\mathbf{x}, t) = 2 \sum_{n=1}^N \tilde{u}_n \cos(\mathbf{k}_n \cdot (\mathbf{x} - t\mathbf{u}_c) + \psi_n + \omega_n t) \boldsymbol{\sigma}_n, \quad (12)$$

where  $\mathbf{u}_c$  is the convection velocity and  $\omega_n$  is the angular frequency of the  $n^{\text{th}}$  mode. As opposed to the convection velocity  $\mathbf{u}_c$ , which is a function of the known local mean flow, the angular frequency  $\omega_n$  is a random variable. Kraichnan [11] treated  $\omega_n$  and  $k_n$  as independent variables; however, aerodynamic noise generation cannot be treated satisfactorily with this supposition. Therefore, Bailly et al. [1] proposed to draw  $\omega_n$  from a distribution associated to a Gaussian probability density function

$$p_n(\omega) = \frac{1}{\omega_{0,n} \sqrt{2\pi}} \exp\left(-\frac{(\omega - \omega_{0,n})^2}{2\omega_{0,n}^2}\right), \quad (13)$$

where the mean angular frequency of the  $n^{\text{th}}$  mode  $\omega_{0,n}$  is connected to the wave number  $k$  by  $\omega_{0,n} = u'k_n$ . Additionally, the authors propose to use the Heisenberg time  $\tau_H \sim (u'k)^{-1}$  as the spectrally local characteristic time. Billson et al. [3] compute the wave number  $k_e$  of the most energetic eddies starting from the turbulence length scale of the RANS solution

$$\Lambda = C_\mu \frac{K^{3/2}}{\epsilon}, \quad (14)$$

where  $C_\mu$  is a closure coefficient of the  $k - \epsilon$  turbulence model. Under the assumption that this length scale is the equal to the integral length scale for isotropic turbulence [13], the following relation holds

$$\Lambda = \frac{\pi}{2u'^2} \int_0^\infty \frac{E(k)}{k} dk. \quad (15)$$

Hence,  $k_e$  can be computed as

$$k_e = \frac{9\pi}{55} \frac{\alpha}{\Lambda}. \quad (16)$$

## 2.1 Filter definition

The following XML-snippet illustrates a typical setting of the SNGR filter.

```
<syntheticTurbulence_SNGR id="synthTurb" tkeCriterion="0.1"
numOfModes="30" inputFilterIds="cfdEnsign" lengthScaleFactor="1.0"
timeScaleFactor="1.0" angularFreqFactor="1.0">
  <incrementModes>equidistant</incrementModes>
  <waveNumBounds minWN="0.1" maxWN="10"/>
  <frequencyBounds minFreq="200" maxFreq="12000"/>
  <TKE resultName="fluidMechTKE"/>
  <TEF resultName="fluidMechTEF"/>
  <localDensity resultName="fluiMechDensity"/>
  <localTemp resultName="fluidMechTemp"/>
  <meanVelocity resultName="fluidMechVelocity"/>
  <output resultName="syntheticTurbVelocity"/>
</syntheticTurbulence_SNGR>
```

- tkeCriterion: only use turbulent kinetic energy (TKE) values when larger than 10%.
- numOfModes:  $N$
- lengthScaleFactor, timeScaleFactor, angularFreqFactor scalars to stretch the space, time, or frequency respectively
- incrementModes: equidistant or logarithmic
- waveNumBounds: minimum and maximum resolve wave number
- frequencyBounds: minimum and maximum resolve frequency
- TKE, TEF (turbulent eddy frequency), localDensity, localTemp (field Temperature), meanVelocity are the field variables that must be supplied by the input.
- output: output field definition.

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