

Creep Cavitation in Nickel-Based Alloys

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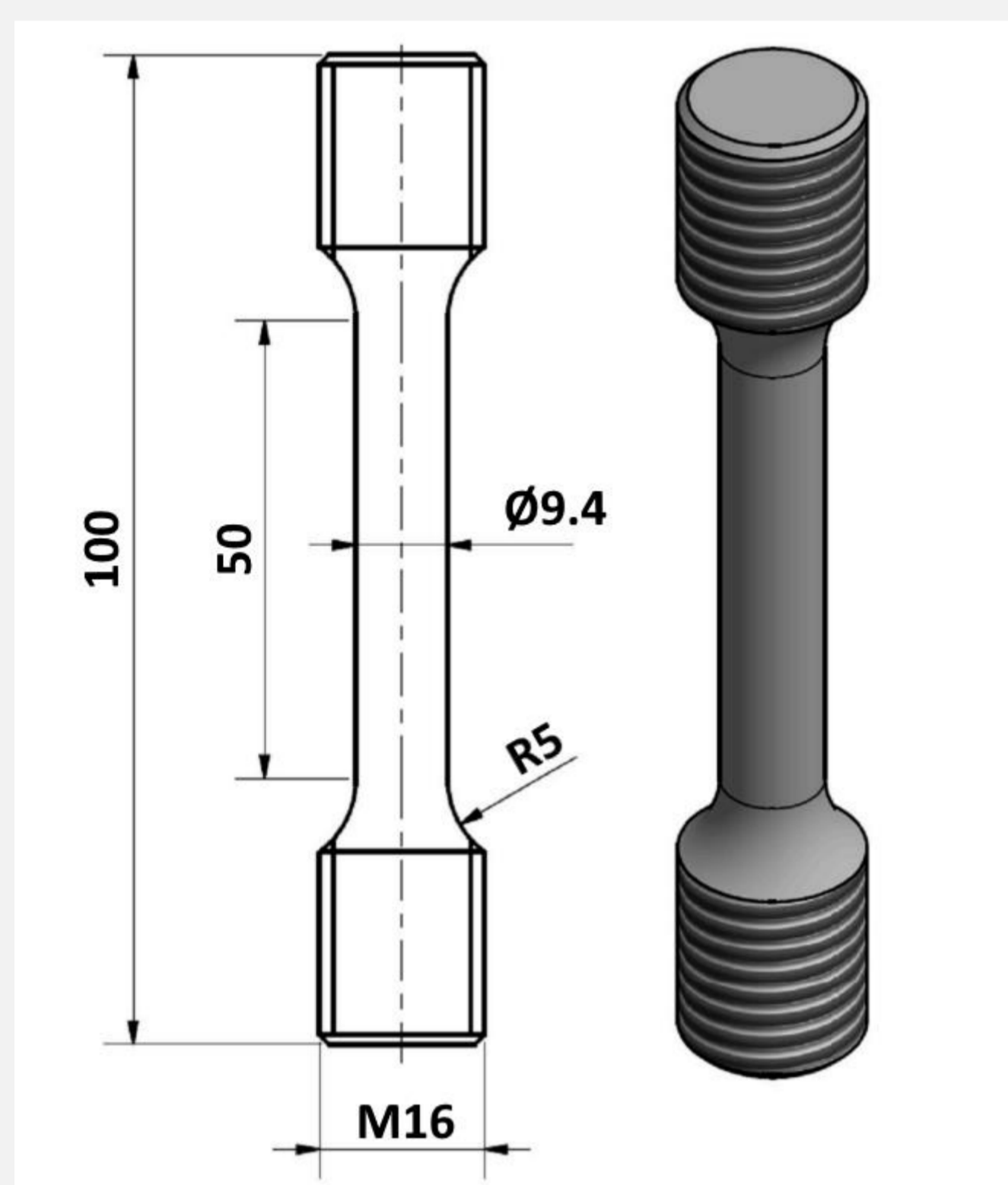
INTRODUCTION

Efforts to reduce the production, operating and environmental costs of thermal power plants require materials that can handle the high operating pressures and temperatures. The current paragons of these materials, nickel-based alloys, still however deform at these high temperatures and stresses, a phenomenon known as creep. During service, vacancies accumulate, mostly at grain boundaries, and form small cavities, which grow slowly and eventually coalesce into large cracks causing the material to rupture. Two mechanisms have been proposed to explain the nucleation of these cavities: Classical Nucleation Theory (CNT) and Grain Boundary Sliding (GBS). Our results support nucleation by the former and growth and coalescence by the latter.

EXPERIMENTAL RESULTS

We crept a specimen (figure 1) of Alloy 617 (chemical composition in Table 1) at 700°C at 170 MPa until it ruptured after 11577 hours.

The 3D volume and analysis of the cavities' directions in the creep specimen were generated using Dragonfly software, Version 2020.2 for Windows (Object Research Systems Inc, Montreal, Canada)



Element	wt%
Ni	Bal
Cr	21.94
Mo	8.64
Co	1.68
Al	1.16
Fe	1.02
Mn	0.04
Cu	0.03
Ti	0.39
Si	0.08
C	0.06
B	0.002

Figure 1: Creep specimen of Alloy 617

Table 1: Composition of Alloy 617

We then investigated the microstructure, looking for cavities and chains of cavities by Scanning Electron Microscopy (Zeiss Ultra 55) and by X-Ray Computer Tomography (Zeiss Xradia 510 Versa and Zeiss Xradia 810 Ultra). The micrographs (figure 2) show the various stages of creep cavitation damage along the grain boundaries.

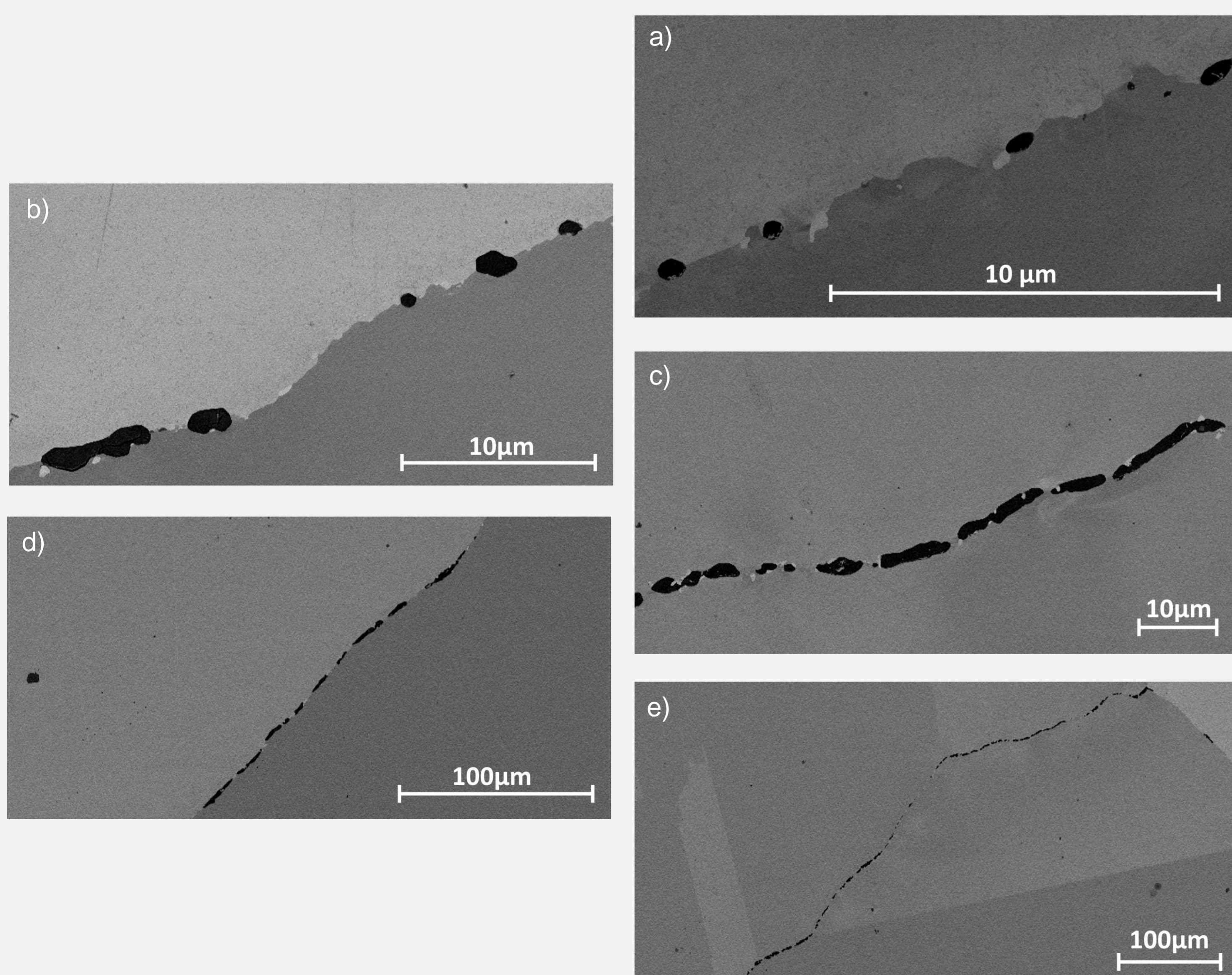


Figure 2: Stages of creep cavitation during creep. Stress was applied in the vertical direction

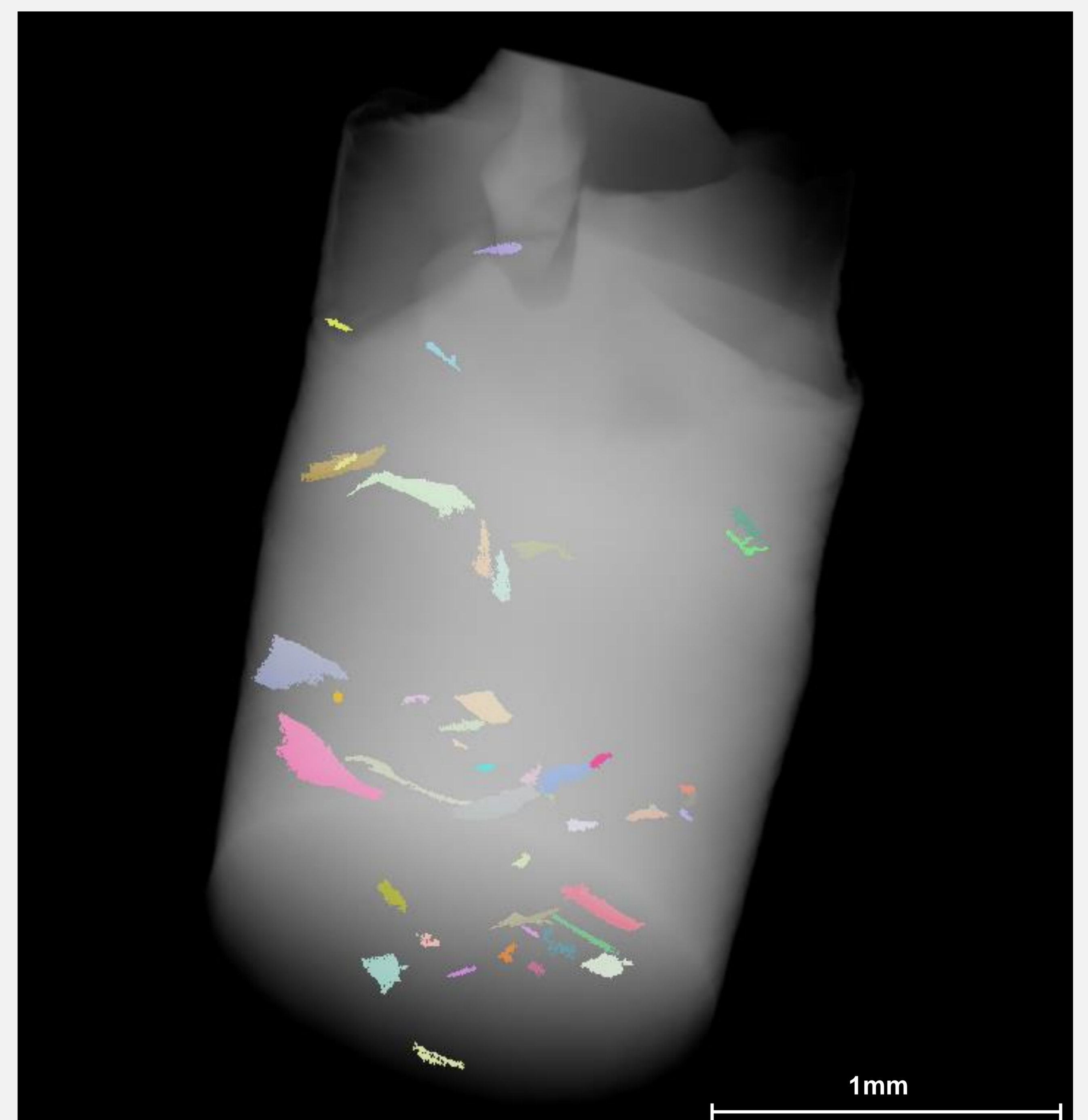


Figure 3: Chains of cavities covering grain boundaries in a fragment (≈ 1.5 mm) of the creep specimen. Stress was applied along the longitudinal axis

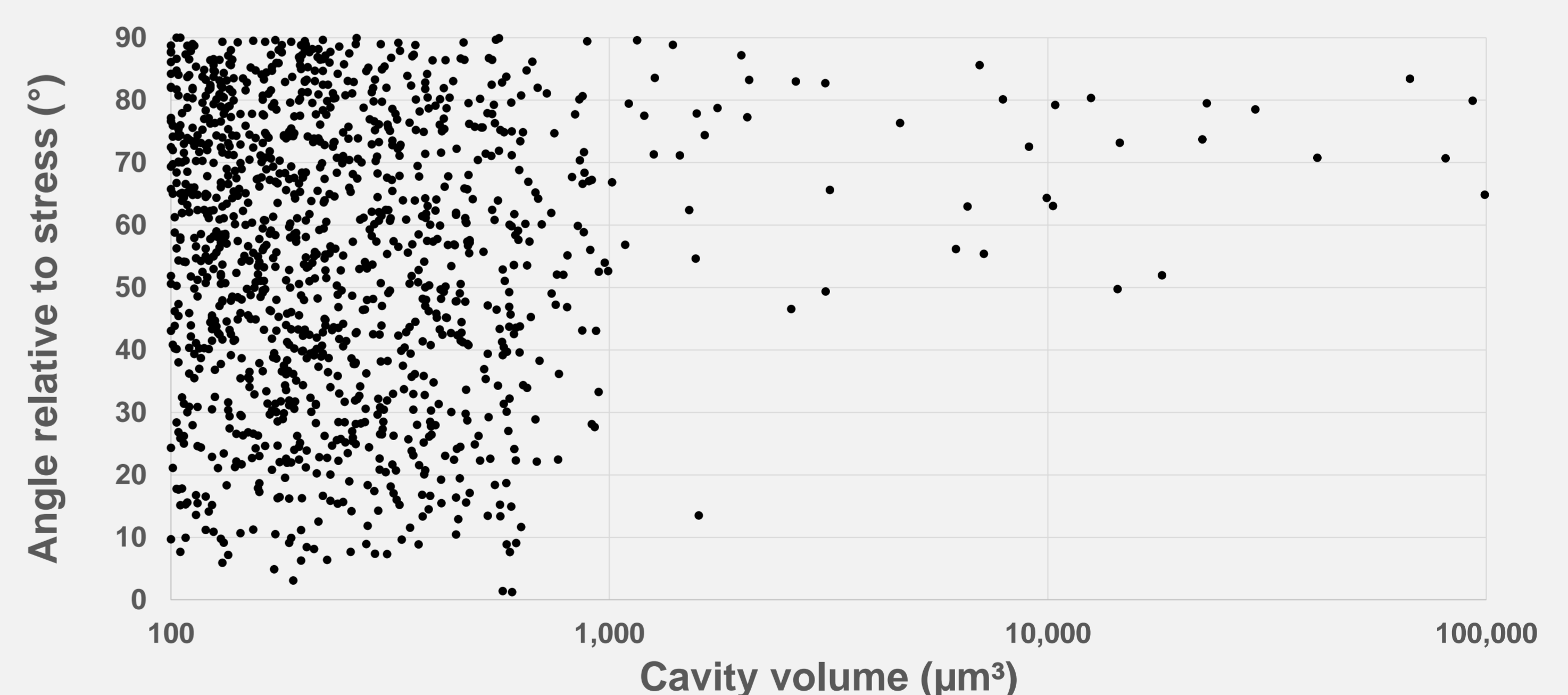


Figure 4: Small cavities grow on any grain boundary, while large chains prefer grain boundaries at oblique angles relative to the principal stress

CONCLUSIONS

The micrographs (Figure 2) and especially the analysis of the cavities in the 3D volume (Figure 4) show small cavities ($<1000\mu\text{m}^3$) evenly distributed along grain boundaries of all orientations. This is consistent with Classical Nucleation Theory which presumes the uniaxial tension as the global driving force for nucleation throughout the microstructure. Large chains of cavities ($>1000\mu\text{m}^3$) grow along grain boundaries which experience more shear stress ($>45^\circ$), which is the driving force for Grain Boundary Sliding. As such it seems that both theories are needed to fully explain creep cavity nucleation and growth which could lead to failure of power plant components.